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U.S. DEPARTMENT OF COMMERCE PATENT AND TRADEMARK OFFICE

ATTORNEY'S DOCKET NUMBER

P/70017-PCT

TRANSMITTAL LETTER TO THE UNITED STATES
DESIGNATED/ELECTED OFFICE (DO/EO/US)
CONCERNING A FILING UNDER 35 U.S.C. 371

U.S. APPLICATION NO. (If known, see 37 CFR 1.5)

09/937746

INTERNATIONAL APPLICATION NO.

PCT/GB00/01112

INTERNATIONAL FILING DATE

March 31, 2000

PRIORITY DATE CLAIMED

April 1, 1999

TITLE OF INVENTION IMPROVEMENTS IN ELECTRICAL MACHINES

APPLICANT(S) FOR DO/EO/US Charles Neville GLEW

Applicant herewith submits to the United States Designated/Elected Office (DO/EO/US) the following items and other information:

1. ☒ This is a **FIRST** submission of items concerning a filing under 35 U.S.C. 371.
2. ☐ This is a **SECOND** or **SUBSEQUENT** submission of items concerning a filing under 35 U.S.C. 371.
3. ☒ This is an express request to begin national examination procedures (35 U.S.C. 371 (f)). The submission must include items (5), (6), (9) and (21) indicated below.
4. ☐ The US has been elected by the expiration of 19 months from the priority date (Article 31).
5. ☒ A copy of the International Application as filed (35 U.S.C. 371(c)(2))
 - a. ☐ is attached hereto (required only if not communicated by the International Bureau).
 - b. ☒ has been communicated by the International Bureau.
 - c. ☐ is not required, as the application was filed in the United States Receiving Office (RO/US).
6. ☐ An English language translation of the International Application as filed (35 U.S.C. 371(c)(2)).
 - a. ☐ is attached hereto.
 - b. ☐ has been previously submitted under 35 U.S.C. 154(d)(4).
7. ☒ Amendments to the claims of the International Application under PCT Article 19 (35 U.S.C. 371(c)(3)).
 - a. ☐ are attached hereto (required only if not communicated by the International Bureau).
 - b. ☒ have been communicated by the International Bureau.
 - c. ☐ have not been made; however, the time limit for making such amendments has NOT expired.
 - d. ☐ have not been made and will not be made.
8. ☐ An English language translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371(c)(3)).
9. ☐ An oath or declaration of the inventor(s) (35 U.S.C. 371(c)(4)).
10. ☐ An English language translation of the annexes to the International Preliminary Examination Report under PCT Article 36 (35 U.S.C. 371(c)(5)).

Items 11 to 20 below concern document(s) or information included:

11. ☐ An Information Disclosure Statement under 37 CFR 1.97 and 1.98.
12. ☐ An assignment document for recording. A separate cover sheet in compliance with 37 CFR 3.28 and 3.31 is included.
13. ☒ A **FIRST** preliminary amendment.
14. ☐ A **SECOND** or **SUBSEQUENT** preliminary amendment.
15. ☐ A substitute specification.
16. ☐ A change of power of attorney and/or address letter.
17. ☐ A computer-readable form of the sequence listing in accordance with PCT Rule 13ter.2 and 35 U.S.C. 1.821 - 1.825.
18. ☐ A second copy of the published international application under 35 U.S.C. 154(d)(4).
19. ☐ A second copy of the English language translation of the international application under 35 U.S.C. 154(d)(4).
20. ☒ Other items or information: PCT/IB/301; 304; 308; 316; 332; PCT/IPEA/408; 409; 416

U.S. APPLICATION NO. (if known, see 37 CFR 1.43) 09/937746		INTERNATIONAL APPLICATION NO. PCT/GB00/01112		ATTORNEY'S DOCKET NUMBER P/70017-PCT	
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21. <input checked="" type="checkbox"/> The following fees are submitted: BASIC NATIONAL FEE (37 CFR 1.492 (a) (1) - (5)) : Neither international preliminary examination fee (37 CFR 1.482) nor international search fee (37 CFR 1.445(a)(2)) paid to USPTO and International Search Report not prepared by the EPO or JPO \$1,000.00 International preliminary examination fee (37 CFR 1.482) not paid to USPTO but International Search Report prepared by the EPO or JPO \$860.00 International preliminary examination fee (37 CFR 1.482) not paid to USPTO but international search fee (37 CFR 1.445(a)(2)) paid to USPTO \$710.00 International preliminary examination fee (37 CFR 1.482) paid to USPTO but all claims did not satisfy provisions of PCT Article 33(I)-(4) \$690.00 International preliminary examination fee (37 CFR 1.482) paid to USPTO and all claims satisfied provisions of PCT Article 33(1)-(4) \$100.00 ENTER APPROPRIATE BASIC FEE AMOUNT =				CALCULATIONS PTO USE ONLY 	
				\$860.00	
Surcharge of \$130.00 for furnishing the oath or declaration later than <input type="checkbox"/> 20 <input type="checkbox"/> 30 months from the earliest claimed priority date (37 CFR 1.492 (e)).				\$0.00	
CLAIMS	NUMBER FILED	NUMBER EXTRA	RATE	\$	
Total claims	24 - 20 =	0	x \$18.00	\$72.00	
Independent claims	5 - 3 =	0	x \$80.00	\$160.00	
MULTIPLE DEPENDENT CLAIM(S) (if applicable)			+ \$270.00	\$1,092.00	
TOTAL OF ABOVE CALCULATIONS =					
<input type="checkbox"/> Applicant claims small entity status. See 37 CFR 1.27. The fees indicated above are reduced by 1/2.					
SUBTOTAL =				\$1,092.00	
Processing fee of \$130.00 for furnishing the English translation later than <input type="checkbox"/> 20 <input type="checkbox"/> 30 months from the earliest claimed priority date (37 CFR 1.492(f)).				\$0.00	
TOTAL NATIONAL FEE =				\$1,092.00	
Fee for recording the enclosed assignment (37 CFR 1.21 (h)). The assignment must be accompanied by an appropriate cover sheet (37 CFR 3.28, 3.31). \$40.00 per property +				\$0.00	
TOTAL FEES ENCLOSED =					
				Amount to be refunded:	\$
				charged:	\$

a. ☒ A check in the amount of \$1,092.00 to cover the above fees is enclosed.

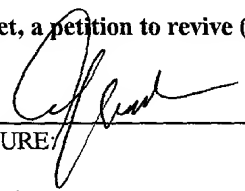
b. ☐ Please charge my Deposit Account No. 11-1145 in the amount of \$_____ to cover the above fees.
A duplicate copy of this sheet is enclosed.

c. ☒ The Commissioner is hereby authorized to charge any additional fees which may be required, or credit any
overpayment to Deposit Account No. 11-1145. A duplicate copy of this sheet is enclosed.

NOTE: Where an appropriate time limit under 37 CFR 1.494 or 1.495 has not been met, a petition to revive (37 CFR 1.137 (a) or (b)) must be filed and granted to restore the application to pending status.

SEND ALL CORRESPONDENCE TO:

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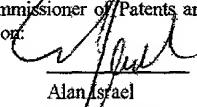

 SIGNATURE
 Alan Israel
 NAME
 27564
 REGISTRATION NUMBER

09/937746

410 Rec'd PCT/PTO 28 SEP 2001

Docket No.: P/70017

PATENTS
IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

I hereby certify that this correspondence is being deposited with the U.S. Postal Service as Express Mail No. EL 337 911 533 US in an envelope addressed to: Box: PCT, Commissioner of Patents and Trademarks, Washington, D.C., 20231, on September 28, 2001
(date) 
Alan Israel
Reg. No. 27,564

International Application No.: PCT/GB00/01112

International Filing Date : March 31, 2000

In re: Application of : Charles Neville GLEW

Deposited : September 28, 2001

For : IMPROVEMENTS IN ELECTRICAL MACHINES

New York, New York
September 28, 2001

PRELIMINARY AMENDMENT

BOX: PCT
Commissioner of Patents and Trademarks
Washington, D.C. 20231

Sir:

Prior to calculation of the filing fee and before examination, kindly amend the above captioned application as follows:

IN THE CLAIMS:

Please cancel claims 1-23, without prejudice.

Please add the new set of claims set forth on the enclosed pages.

IN THE ABSTRACT:

Delete the "Abstract" on the PCT cover sheet and replace it with the "Abstract of the Disclosure" set forth on a separate sheet attached hereto.

REMARKS

An abstract has been provided on a separate sheet; and the claims have been amended to conform to U.S. practice.

Wherefore, an early action on the merits is earnestly solicited.

Respectfully submitted,

KIRSCHSTEIN, OTTINGER, ISRAEL & SCHIFFMILLER, P.C.

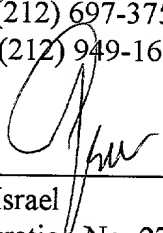
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ABSTRACT OF THE DISCLOSURE

A composite conductor comprises strands of conductor material forming a conductor bundle of generally rectangular shape, the strands being insulated from each other within the bundle. An insulating sleeve of homogeneous polymeric material surrounds the conductor bundle; the insulating sleeve also having a rectangular shape. The polymeric material of the sleeve is filled with at least one insulating filler material which conducts heat more efficiently than the polymer alone, and a coating of conductive material from a corona shield on the inner and outer surfaces of the insulating sleeve. By virtue of its construction and the materials it uses, the composite conductor provides a high efficiency winding for the stator of an electrical machine. The invention also includes a stator having a winding comprising the composite conductor and manufacturing methods for the composite conductor and the stator. —

PROPOSED NEW CLAIMS

24. A composite conductor for use as a winding of a high voltage electrical machine, comprising:

a) a plurality of strands of conductor material forming a conductor bundle which in cross-section is of generally rectangular shape, the strands being insulated from each other within the bundle;

b) an insulating sleeve of substantially homogeneous polymeric material surrounding the conductor bundle, the insulating sleeve also having a generally rectangular shape in cross-section, and the polymeric material being filled with at least one electrically insulating filler material which conducts heat more efficiently than the polymer alone; and

c) conductive material forming a corona shield coating at inner and outer surfaces of the insulating sleeve.

25. The composite conductor according to claim 24, the conductor bundle having radiused corners to minimize electrical stress concentrations.

26. The composite conductor according to claim 25, the corners having radius dimensions up to about 5 mm.

27. The composite conductor according to claim 26, the radius dimensions being between 2-3 mm.

28. The composite conductor according to claim 24, the insulating sleeve having substantially rectilinear corners.

29. The composite conductor according to claim 28, the corners of the insulating sleeve having a radius of not more than about 1 mm.

30. The composite conductor according to claim 24, the strands in the bundle of conductor material being collectively twisted around a longitudinal centerline of the conductor bundle, thereby to reduce winding losses from eddy currents.

31. The composite conductor according to claim 24, the at least one insulating filler material in the polymer insulating sleeve being at least one of a metallic oxide and a metallic nitride.

32. The composite conductor according to claim 24, the polymeric sleeve material comprising a high-temperature resistant polymer.

33. The composite conductor according to claim 32, the polymeric sleeve material comprising at least one of fluoropolymer and an aromatic polymer.

34. The composite conductor according to claim 24, the conductive coating material comprising at least one of a graphitic and a silicon based material.

35. The composite conductor according to claim 34, the conductive coating material comprising at least one of a high-temperature resistant polymer and a paint material which has sufficient of the conductive material incorporated therein to render it conductive.

36. The composite conductor according to claim 34, the conductive coating material being an extruded film.

37. The composite conductor according to claim 24, the conductor strands being insulated from each other by means of a high-temperature resistant insulating coating applied to each strand during manufacture of the strands before their incorporation into the conductor bundle.

38. The composite conductor according to claim 24, the conductor strands being insulated from each other by means of impregnation of the conductor bundle with a curable high-

temperature resistant insulating material during incorporation of the strands into the conductor bundle.

39. A process of making a composite conductor, comprising the steps of:

a) gathering together a plurality of strands of conductor material into a conductor bundle and twisting the bundled strands bodily about a longitudinal centerline of the bundle to form a twisted conductor bundle;

b) impregnating the conductor bundle with a curable high-temperature resistant insulating material, the impregnation occurring one of simultaneously with the gathering and twisting process and subsequent thereto;

c) applying a coating of conductive material to an exterior of the twisted conductor bundle to form a first, inner, corona shield;

d) extruding an insulating sleeve of homogeneous polymeric material onto the coating of conductive material on the conductor bundle, the polymeric material having been previously filled with at least one insulating filler material which conducts heat more efficiently than the polymer alone;

e) applying a coating of conductive material to an outer surface of the insulating sleeve to form a second, outer, corona shield; and

f) providing each strand of the conductor material with an insulating coating by at least one of coating the strands before the formation of the conductor bundle, and coating the strands during the impregnating step.

40. The process according to claim 39, in which after twisting of the bundle, the bundle is formed to a predetermined cross-sectional shape.

41. The process according to claim 40, in which the predetermined cross-sectional shape is rectangular.

42. The process according to claim 39, in which the impregnated conductor bundle is partially cured before the coating of conductive material is applied to the exterior of the conductor bundle.

43. A stator for a rotary electrical machine, comprising: a laminated steel core provided with a plurality of radially oriented slots extending longitudinally of the stator, each slot housing a winding comprising a plurality of turns of a single length of a composite conductor, successive turns of the composite conductor being in contact and in radial registration with each other, the composite conductor including

a) a plurality of strands of conductor material forming a conductor bundle which in cross-section is of generally rectangular shape, the strands being insulated from each other within the bundle;

b) an insulating sleeve of substantially homogeneous polymeric material surrounding the conductor bundle, the insulating sleeve also having a generally rectangular shape in cross-section, and the polymeric material being filled with at least one electrically insulating filler material which conducts heat more efficiently than the polymer alone; and

c) conductive material forming a corona shield coating at inner and outer surfaces of the insulating sleeve.

44. A stator for a rotary electrical machine, comprising: a laminated steel core provided with a plurality of radially oriented slots extending longitudinally of the stator, each slot housing a winding comprising a plurality of turns comprising a plurality of lengths of a composite

conductor, successive turns of the composite conductor being in contact and in radial registration with each other, the composite conductor including

a) a plurality of strands of conductor material forming a conductor bundle which in cross-section is of generally rectangular shape, the strands being insulated from each other within the bundle;

b) an insulating sleeve of substantially homogeneous polymeric material surrounding the conductor bundle, the insulating sleeve also having a generally rectangular shape in cross-section, and the polymeric material being filled with at least one electrically insulating filler material which conducts heat more efficiently than the polymer alone; and

c) conductive material forming a corona shield coating at inner and outer surfaces of the insulating sleeve.

45. The stator according to claim 43, the winding being retained in its slot by a high thermal conductivity, electrically insulating retaining means fixed in the radially outer end of the slot.

46. The stator according to claim 44, the winding being retained in its slot by a high thermal conductivity, electrically insulating retaining means fixed in the radially outer end of the slot.

47. A method of making a stator for a rotary electrical machine, comprising the steps of: providing a laminated steel core with a plurality of radially oriented slots extending longitudinally of the stator, each slot housing a winding comprising a plurality of turns of a single length of a composite conductor, successive turns of the composite conductor being in contact and in radial registration with each other, the composite conductor including a plurality of strands of

conductor material forming a conductor bundle which in cross-section is of generally rectangular shape, the strands being insulated from each other within the bundle, providing an insulating sleeve of substantially homogeneous polymeric material surrounding the conductor bundle, the insulating sleeve also having a generally rectangular shape in cross-section, the polymeric material being filled with at least one electrically insulating filler material which conducts heat more efficiently than the polymer alone; providing conductive material forming a corona shield coating at inner and outer surfaces of the insulating sleeve; in which the conductor bundle has been impregnated with a curable high-temperature insulation material and is wound onto the stator core while the curable high-temperature insulation material is only partly cured, attaching support means to the composite conductor where it is unsupported by the stator slots, and heat treating the completed stator to cure the curable high-temperature insulation material and produce a rigid stator winding.

AMENDED CLAIMS

[received by the International Bureau on 6 September 2000 (06.09.00);
original claims 24-26 cancelled; original claim 8 amended;
claims 11-22 renumbered as claims 12-23 other claims unchanged (3 pages)]

7. A composite conductor according to any preceding claim, the strands in the bundle of conductor material being collectively twisted around the longitudinal centreline of the conductor bundle, thereby to reduce winding losses from eddy currents.

5

8. A composite conductor according to any preceding claim, the at least one insulating filler material in the polymer insulating sleeve being a metallic oxide and/or a metallic nitride.

10 9. A composite conductor according to any preceding claim, the polymeric sleeve material comprising a high-temperature resistant polymer.

10. A composite conductor according to claim 9, the polymeric sleeve material comprising a fluoropolymer or an aromatic polymer.

15

11. A composite conductor according to any preceding claim, the conductive coating material comprising a graphitic or silicon based material.

12. A composite conductor according to claim 11, the conductive coating material
20 comprising a high-temperature resistant polymer or paint material which has sufficient of the conductive material incorporated therein to render it conductive.

13. A composite conductor according to claim 11 or claim 12, the conductive coating material being an extruded film.

25

14. A composite conductor according to any preceding claim, the conductor strands being insulated from each other by means of a high-temperature resistant insulating coating applied to each strand during manufacture of the strands before their incorporation into the conductor bundle.

30

15. A composite conductor according to any one of claims 1 to 13, the conductor strands being insulated from each other by means of impregnation of the conductor bundle with a curable high-temperature resistant insulating material during incorporation of the strands into the conductor bundle.

5

16. A process for making a composite conductor, comprising the steps of:

gathering together a plurality of strands of conductor material into a conductor bundle and twisting the bundled strands bodily about a longitudinal centreline of the bundle to form a twisted conductor bundle,

10 impregnating the conductor bundle with a curable high-temperature resistant insulating material, the impregnation occurring one of simultaneously with the gathering and twisting process and subsequent thereto,

applying a coating of conductive material to the exterior of the twisted conductor bundle to form a first, inner, corona shield,

15 extruding an insulating sleeve of homogeneous polymeric material onto the coating of conductive material on the conductor bundle, the polymeric material having been previously filled with at least one insulating filler material which conducts heat more efficiently than the polymer alone, and

20 applying a coating of conductive material to the outer surface of the insulating sleeve to form a second, outer, corona shield;

wherein each strand of conductor material is provided with an insulating coating by at least one of coating the strands before the formation of the conductor bundle, and coating the strands during the impregnation step.

25 17. A process according to claim 16, in which after twisting of the bundle, the bundle is formed to a predetermined cross-sectional shape.

18. A process according to claim 17, in which the predetermined cross-sectional shape is rectangular.

30

19. A process according to any one of claims 16 to 18, in which the impregnated conductor bundle is partially cured before the coating of conductive material is applied to the outside of the conductor bundle.

5 20. A stator for a rotary electrical machine, comprising a laminated steel core provided with a plurality of radially oriented slots extending longitudinally of the stator, each slot housing a winding comprising a plurality of turns of a single length of a composite conductor constituted according to claim 1, successive turns of the composite conductor being in contact and in radial registration with each other.

10

21. A stator for a rotary electrical machine, comprising a laminated steel core provided with a plurality of radially oriented slots extending longitudinally of the stator, each slot housing a winding comprising a plurality of turns comprising a plurality of lengths of a composite conductor constituted according to claim 1,
15 successive turns of the composite conductor being in contact and in radial registration with each other.

20

22. A stator according to claim 20 or claim 21, the winding being retained in its slot by a high thermal conductivity, electrically insulating retaining means fixed in the radially outer end of the slot.

25

23. A method of making a stator constituted according to claim 21 or claim 22, in which the conductor bundle has been impregnated with a curable high-temperature insulation material and is wound onto the stator core while the curable high-temperature insulation material is only partly cured, attaching support means to the composite conductor where it is unsupported by the stator slots, and heat treating the completed stator to cure the curable high-temperature insulation material and produce a rigid stator winding.

4/pts

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IMPROVEMENTS IN ELECTRICAL MACHINES

This invention relates to electrical machines and in particular to insulated electrical conductors suitable for use as excitation windings on the stators of high voltage
5 electrical machines, for example, machines operating at voltages greater than 3KV.

Known types of excitation winding for the stators of such machines generally comprise solid rectangular copper conductors which are electrically insulated from each other and from an earthed laminated steel core on which they are wound. Materials used to
10 insulate the conductors are chosen so as to have properties - such as thickness, thermal conductivity, dielectric strength, and permittivity - which are appropriate to the size of the machine, applied voltage and temperature rise.

The power output of a rotating electrical machine (whether a motor or a generator) is
15 a function of the properties of the laminated magnetic steel core, the excitation windings and their operating temperature. An "output coefficient" or "specific torque coefficient" of such machines is often quoted as a useful means of comparing the power outputs of machines of differing design. Its units are torque per unit volume and it may be derived by dividing the machine's power output by the volume of the stator
20 within the air-gap periphery.

Having been the subject of industrial manufacture for over 100 years, rotating electrical machines are considered a mature product using mature technologies. Over the century of production the materials and processes used in the construction have
25 evolved slowly resulting in a steady increase in output coefficient (about 3.0% per annum) for the most popular machines. Recently, their evolutionary progress has slowed down and has now reached a plateau, suggesting that further development is either unlikely or will be very slow.

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It is necessary to externally insulate the stator windings of such machines from each other and the stator core. It is also necessary to internally insulate the windings by insulating the conductors from each other within the winding. The insulation materials presently used to perform the insulation function have only limited ability to withstand
5 high temperatures, with modest electric strength properties and generally poor thermal conductivity. Furthermore, during operation of the machines, heat is generated due to electrical losses in the winding conductors, but the poor thermal conductivity of the insulation materials results in poor transfer of the heat, and this in turn inhibits the output coefficients of the machines on which the insulation materials are used.

10

Since there are only small differences between the stator winding insulation systems used currently by leading manufacturers of machines, the thermal and dielectric performance of such systems is similar. Typically, all use combinations of mica, polyester film and woven glass materials impregnated with synthetic resins. The mica is
15 used in the form of a so-called "paper" which is supported by either polyester film or woven glass and is wrapped around the conductors to insulate them from external contact. To complete the insulation process, they are vacuum pressure impregnated with the synthetic resin (for example, an epoxide resin) as the last process after positioning the windings into the stator.

20

It is an object of the present invention to improve the output coefficients of electrical machines and hence reduce their capital cost per KW output of electrical energy by increasing the heat transfer capability of their stator conductor windings. This is achieved in the invention by means of a novel type of composite conductor.

25

According to the present invention, a composite conductor for use as a winding of a high voltage electrical machine comprises:

a plurality of strands of conductor material forming a conductor bundle which in cross-section is of generally rectangular shape, the strands being insulated from each
30 other within the bundle,

- 3 -

an insulating sleeve of substantially homogeneous polymeric material surrounding the conductor bundle; the insulating sleeve also having a generally rectangular shape in cross-section and the polymeric material being filled with at least one electrically insulating filler material which conducts heat more efficiently than the polymer alone, and

conductive material forming a corona shield coating at the inner and outer surfaces of the insulating sleeve.

The conductor bundle is impregnated with a curable high-temperature resistant insulating material, such as a synthetic resin or polymer material, whereby the cured composite conductor is rendered sufficiently strong and rigid to enable its use in the windings of electrical machines.

It should be noted that the term "rectangular" as used herein includes shapes which are square (having four sides all of substantially equal dimensions) and rectangles and squares having rounded corners.

A composite conductor in accordance with the invention, by virtue of its construction and the materials it uses, provides a high efficiency winding for the stator of an electrical machine. Due to its filler material(s), the insulating sleeve not only has superior dielectric strength properties which permits operating at reduced sleeve wall thickness and/or increased electric stress, but also has much higher thermal conductivity and thermal capability (temperature resistance) than known windings. The higher thermal conductivity permits a considerable increase in the heat transfer capability from the composite conductor into the stator core, which may be cooled by heat exchange with ducted airstreams. Furthermore, insulation of the conductor strands from each other substantially reduces high frequency eddy current losses in the stator winding, and the conductive surface coating on the insulation sleeve contributes to enabling safe operation at higher electric stresses at the surface of the sleeve. The

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net result of the above is that the output coefficient is substantially increased and hence the capital cost of the delivered power is substantially decreased.

5 Preferably, the corners of the conductor bundle's rectangular shape are radiused to minimise electrical stress concentrations. The radius dimension may be up to 5 mm., preferably between 2-3 mm., but it is preferred that the corners of the insulating sleeve are substantially rectilinear, having a radius of not more than about 1mm.

10 Preferably, the strands of conductor material are collectively twisted around the longitudinal centreline of the conductor bundle in a similar manner to which the strands in a rope are twisted about the longitudinal centreline of the rope. This angular/spatial transposition of the strands of conductor material longitudinally of the bundle due to its twist inherently cancels eddy currents as they arise, substantially reducing or eliminating the associated losses.

15 The at least one insulating filler material in the polymer insulating sleeve is preferably a metallic oxide and/or a metallic nitride.

20 The polymeric sleeve material preferably comprises a high temperature polymer, e.g. a polymer selected from the groups comprising fluoropolymers or aromatic polymers, and the conductive coating material for reducing electric stress variations at the surfaces of the composite conductor may comprise a graphitic or silicon-based material, preferably a high-temperature resistant polymer or paint material which has sufficient of the conductive material incorporated therein to render it conductive.

25 Preferably the strands of conductor material comprise copper, but other materials may be useable, such as aluminium or silver. Whatever the material from which the conductor strands are made, it is preferred they are insulated from each other by means of a coating of high-temperature resistant synthetic resin or polymer material on each
30 strand. This may be achieved either by impregnation of the conductor bundle with a

- 5 -

resin or precursor polymer material in its uncured state, or perhaps more conveniently and reliably by using conductor strands that have been previously manufactured with an insulating coating before being incorporated into the conductor bundle. Both these conductor coating techniques are well known in the art.

5

The invention further envisages a process for making the above composite conductor, comprising the steps of:

gathering together a plurality of strands of conductor material to form a conductor bundle,

10 impregnating the conductor bundle with a curable high-temperature resistant insulating material, the impregnation occurring one of simultaneously with the gathering process and subsequent thereto,

applying a coating of conductive material to the exterior of the twisted conductor bundle to form a first, inner, corona shield,

15 extruding an insulating sleeve of homogeneous polymeric material onto the coating of conductive material on the conductor bundle, the polymeric material having been previously filled with at least one insulating filler material which conducts heat more efficiently than the polymer alone, and

20 applying a coating of conductive material to the outer surface of the insulating sleeve to form a second, outer, corona shield;

wherein each strand of conductor material is provided with an insulating coating by at least one of coating the strands before the formation of the conductor bundle, and coating the strands during the impregnation step.

25 We prefer that the conductor bundle is formed into a generally rectangular shape during or subsequent to the gathering process. We further prefer that subsequent to the formation of the conductor bundle, the bundled strands are twisted bodily about a longitudinal centreline of the bundle to form a twisted conductor bundle.

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Whereas it is known to impregnate the insulating wrappings of bar conductor windings with synthetic resin after they have been assembled onto the stator, then partially or wholly to cure the resin, it is envisaged that in the present invention, impregnation occurs before the composite conductor is wound onto the stator, the composite
5 conductor then being wound onto the stator while the resin or precursor polymer material is uncured or only partly cured. This facilitates the impregnation process while allowing easy manipulation of the composite conductor during the stator winding process before the resin is fully cured.

10 The invention also includes a stator for a rotary electrical machine comprising a laminated steel core provided with a plurality of radially oriented slots extending longitudinally of the stator, each slot housing a winding comprising either a plurality of turns of a single length of the above composite conductor, or a plurality of turns comprising a plurality of lengths of the above composite conductor, successive turns of
15 the composite conductor being in contact and in radial registration with each other. The winding is retained in its slot, preferably by a high thermal conductivity, electrically insulating retaining means fixed in the radially outer end of the slot. Preferably, the retaining means is a filled polymer composition having relatively high thermal conductivity compared to the polymer in its unfilled state.

20 The retaining means may comprise an extrusion which is forced into the end of the slot.

It should be understood that the materials mentioned herein in connection with
25 composite conductors according to the invention are best estimates of which materials will probably be suitable.

Exemplary embodiments of the invention will now be described with reference to the accompanying drawings, in which:

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Figure 1 is a perspective view of part of the inside of a stator of a rotary electrical machine provided with a conventional winding;

Figure 2 is a cross-section of a composite conductor according to the present invention;

5 Figure 3 is a cross-section of an alternative composite conductor according to the present invention;

Figure 4 is a radial section through part of a stator according to the invention, showing a stator slot containing a winding comprising six turns of the composite conductor shown in Figure 2;

10 Figure 5 is a diagrammatic representation of a process for manufacturing a composite conductor according to the invention.

Referring to Figure 1, there is shown the inner circumference of one end of a stator 10 of an A.C. electrical machine. The stator is intended to encircle the rotor (not shown) of the electrical machine. As is conventional, the stator body is composed of a large number of steel laminations and is formed with a large number of radially oriented slots 12 which extend longitudinally of the stator body.

Each slot 12 houses an excitation winding 14, successive "turns" 14A, 14B of which contact each other and are in radial registration within their slot. The windings are retained in their slots by wedges 16, made of a suitable polymer insulation material, such as filled epoxide resin. During manufacture of the stator, wedges 16 are forced into position within the mouths of the slots 12.

25 The loops or "turns" of the windings each comprise solid rectangular copper conductor bars 14A, 14B which are pre-formed to the correct shape to enable their installation into the stator slots. The conductor bars are electrically insulated from each other and from the earthed steel core by wrappings of mica paper on polyester support film, the wrappings being pressure-impregnated with epoxide resin and cured later.

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To enable the construction of the stator winding 14 from pre-formed lengths of conductor bar, each turn of the winding consists of a plurality of lengths of conductor bar whose ends 15 projecting from the stator core are bent at compound angles as shown, these ends being brazed or otherwise securely joined together in electrical
5 contact (not shown) to complete the turn. The ends of radially adjacent conductor bars 14A, 14B are bent in opposing directions.

As Figure 1 shows, where the ends of the conductor bars 14A, 14B, etc., project from the ends of the slots 12, packing blocks 18, 20 are inserted between adjacent
10 conductor bars, packing blocks 18 being adjacent the end of the stator core and packing blocks 20 being spaced away from the stator core. Various of the packing blocks 18, 20 and the bent portions of some of the conductor bars 14A and 14B have been removed at the lower left of Figure 1 to show the construction more clearly. The
15 packing blocks are moulded to shape, being made up from glass cloth bags containing glass mat laminate filler pieces impregnated with epoxide resin. Packing blocks 20 are bound to the adjacent conductor bars with glass fibre tape 22.

After assembly of the stator winding and insertion of the packing blocks, assembly of the stator is completed by tying the bent portions 15 of the conductor bars 14A, 14B,
20 to support rings 24, 26 using glass fibre cord 28. The packing blocks and the support rings provide support to the ends of the conductor bars and prevent vibration during service. Finally, the stator assembly is heat-treated at an appropriate curing temperature for its resin-impregnated portions, this temperature being below that
25 which would cause deterioration of the polyester film component of the conductor wrappings.

Turning now to Figure 2, a composite conductor 30 is shown in cross-section and is intended to be used as a stator winding of a high voltage electrical machine, thereby substituting for the wrapped solid conductor bars 14A, 14B of Figure 1. Unlike the
30 solid conductor bars, however, the core of composite conductor 30 comprises a large

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number of strands 31 of conductor material forming a conductor bundle 32. Preferably, the strands 31 of conductor material comprise copper, but other materials may be useable, such as aluminium (cheaper, but not such a good electrical conductor as copper) or silver (expensive, but a better electrical conductor). A typical dimension for
5 an individual strand of conductor material is likely to be of the order of 0.1mm, so it will be appreciated that the number of strands 31 needed to form a conductor bundle 32 is likely to be much larger than that diagrammatically indicated in Figure 2, and their cross-sections will consequently appear smaller relative to the total cross-section of the composite conductor 30.

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Conductor bundle 32, although of generally rectangular shape, has rounded corners 34 to minimise electrical stress concentrations during operation of the electrical machine. The dimensions of the conductor bundle's corner radii R are in the range 0.5 to 5 mm.; 2-3 mm. may be optimum.

15

To reduce high frequency eddy current losses in the stator winding, the bundle of copper strands 32 is bodily twisted around the longitudinal centreline C of the composite conductor 30 in a similar manner to which the fibres in a rope are twisted about the longitudinal centreline of the rope. It should be noted that the spatial
20 transposition of the strands of conductor material longitudinally within the bundle due to its twist inherently cancels eddy currents as they arise.

An insulating sleeve 36 of high temperature polymer material (e.g., a fluoropolymer or an aromatic polymer) surrounds the conductor bundle. In accordance with the
25 invention, the polymer is homogeneously filled with an insulating material which conducts heat more efficiently than the polymer alone. This is explained further below. The insulating sleeve has a rectangular shape in cross-section, but unlike the shape adopted for the conductor bundle, it is preferred that the corners of the insulating sleeve are not substantially rounded, i.e. the long and short sides of the insulating
30 sleeve meet substantially at right angles. However, there may be a small radius present,

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say up to about 1mm., due to the manufacturing process and the need to apply a corona shield coating evenly to the surface of the insulation sleeve. The total width W and height H of the insulating sleeve 36 is substantially uniform in the lateral and lengthwise directions of the composite conductor. The sleeve's wall thickness T1 is
5 similarly uniform, except of course in the regions adjacent the rounded corners 34 of the conductor bundle 32.

Thickness T1 should ideally be as small as possible consistent with adequate electrical insulation properties, because a thin wall for the sleeve 36 enables more rapid
10 conduction of heat away from the bundle of conductor strands 32 and also allows a larger conductor bundle to be included in the composite conductor for the same overall size of composite conductor. The latter point is illustrated by reference to Figure 3, which shows an alternative embodiment of the invention in which the thickness T2 of the sleeve is about twice that of thickness T1 in Figure 2. It will be noticed that the
15 number of conductor strands 31 that can be included in the composite conductor is much less in Figure 3 than in Figure 2.

Ordinary polymer sleeves for electric cables are extruded onto the conductor or conductor bundle by means of an extrusion head through the centre of which runs the
20 conductor to which the sleeve is applied. This is a well known and understood process. A polymer sleeve having a wall thickness of about 0.1mm can be produced by known extrusion processes and it is preferred that the thickness of the polymer sleeve in the invention (excluding the corner regions) should be in the range 0.4 to 2.00mm. For example, a typical value for T1 could be about 0.5mm, preferably 0.65mm, and a
25 typical value for T2 could be about 1mm.

In order to permit operation of the composite conductor 30 with as small a value of T1 as possible, the invention provides that the polymeric material from which the sleeve 36 is made is homogeneously compounded with one or more powdered materials
30 which conduct heat more efficiently than the polymer alone. These materials may be

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metallic oxide or metallic nitride fillers, such as aluminium oxide or aluminium nitride. As a result, the insulating sleeve 36 not only has superior dielectric strength properties which permits operating at reduced thickness, but also has much higher thermal conductivity and temperature resistance than known windings. The approximate
5 volume ratio of polymer to filler material may be 10% to 75%.

To obtain low eddy current losses and hence good electrical efficiency of the composite conductor 30 in its role as a current carrying stator winding in an electrical machine, the individual conductor strands 31 in the conductor bundle 32 are insulated
10 from each other according to the invention. As discussed in more detail below, this can be achieved by impregnating the conductor bundle with a synthetic resin material, such as an epoxide resin, and/or using conductor strands that have been previously provided with an insulating coating. Such pre-coated wires are routinely used in the production of windings for small electrical machines, being wound straight onto a rotor or stator.

15 Before or during the application of the insulating sleeve to the conductor bundle a thin coating of conductive material e.g., a graphitic or silicon-based material, such as a carbon-filled high-temperature resistant polymer, is applied so as to form a corona protective shield on the inside surface of the of the extruded polymer, i.e., at the
20 interface between the insulating sleeve and the conductor bundle. During or after the application of the insulating sleeve to the conductor bundle, a thin coating of the same or a similar conductive material is applied to the outside surface of the insulating sleeve so as to form a corona protective shield thereon. The external coating is indicated by the dotted line 38 surrounding the sleeve 36 in Figure 2 (the inner corona shield is not
25 shown). The purpose of the conductive coating material is to equalise the electric stresses on the surface of the composite conductor during operation of the electrical machine and thereby avoid localised breakdown of the insulation afforded by the insulating sleeve 36. We have found that both inside and outside surfaces of the insulating sleeve should be provided with the conductive corona shield coating to

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provide good equalisation of the electric stresses at the surface of the composite conductor.

A suitable thickness for the inner and outer corona shields is in the range about 0.1 to 0.3mm, preferably at the lower end of this range. As already stated, a polymer film of this thickness is known to be extrudable and therefore the inner and outer corona shields may be applied by means of extrusion, as hereafter described. Alternatively, the inner corona shield may be applied by winding a thin tape of the conductive material onto the conductor bundle before the insulating sleeve is applied thereto and the outer corona shield may be applied by winding a thin tape onto the outside of the insulating sleeve after the insulating sleeve has been applied to the conductor bundle. As yet a further alternative, the corona shields may be applied in the manner of a coat of paint; for instance, before application of the insulating sleeve to the conductor bundle, the latter may pass through a bath of the corona shield material held as a suspension or solution in a suitable liquid and after the insulating sleeve has been applied it may similarly be passed through such a bath. However, in such a process it will be necessary to ensure that the inner corona shield has adequately dried or cured to form a flexible high temperature resistant coating before application of the insulating sleeve to the conductor bundle occurs. Similarly, the outer corona shield coating must have dried or cured to form a flexible high temperature resistant coating before further handling of the composite conductor occurs, such as winding it into the slots of the electrical machine.

To facilitate the impregnation process while allowing easy manipulation of the composite conductor during the process of producing the winding on the stator core, the composite conductor is impregnated before the composite conductor is wound onto the stator and fully cured only after it has been wound onto the stator. As explained later, impregnation may occur at the time when the individual strands of conductor material are gathered together and consolidated into the conductor bundle, before application of the insulating sleeve. We prefer then to partially cure the resin, so

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that the composite conductor is still flexible enough to be wound directly onto the stator, with optional intervening storage on a drum for later use. The completed stator is heat-treated at a temperature below that at which deterioration of the filled polymer sleeve and the corona shield occurs, thereby fully curing the resin to make the finished stator winding rigid.

Turning now to Figure 4, it is shown how the composite conductor 30 of Figure 2 may be used to form a complete stator winding. The stator 40 of a rotary electrical machine comprises a laminated steel core 42 provided with radially oriented slots extending longitudinally of the stator. In the broken-away sectional view, only one of the slots 44 is shown. It houses a winding 46 comprising a plurality of turns or loops of the composite conductor 30. Each turn conveniently comprises a single length of the composite conductor, or alternatively, two or more shorter lengths of composite conductor may be spliced together to complete one turn. As can be seen, successive turns 30A, 30B, etc, of the composite conductor are in contact and in radial registration with each other. It should be noted that the rectangular shape of the composite conductor minimises air voids in the finished winding, enabling geometrically exact production of the winding without pre-forming of rigid bar conductors, as was necessary in the prior art. The winding is retained in its slot 44 by a high thermal conductivity, electrically insulating retaining wedge 48 fixed in the radially outer end of the slot. The wedge may be an extrusion comprising a filled polymer material, such as an epoxide resin, and may be driven into the slot from the end face of the stator.

In connection with the rectangular shape of the conductor bundle and the insulating sleeve, it should be particularly noted that besides the better packing characteristics of the composite conductors in the machine slots, the extra thickness T3-T1 (Figure 2) of the insulation at the corner of the conductor bundle effectively reduces the electric stress at the corner to approximately the same value as that on the flat sides of the

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conductor bundle. Such reduction in peak electric stresses in the windings contributes to an ability of the machine to operate at higher loadings.

During production of the stator, the inherent flexibility provided by the polymer insulation sleeve, the thin corona shield coatings, the thin conductor strands and the uncured or partially cured resin on the conductor strands, permits ease of positioning of the conductor in the slots in the stator core to form a winding. However, after heat-treatment to cure the resin (curing being at a temperature lower than the temperature at which the filled polymer insulation sleeve and the corona shield coatings begin to deteriorate), the rigidity provided by the fully cured resin on the conductor strands enables the finished stator winding to withstand the operational impressed forces. Note that where the composite conductor winding 30 is not within the slots 44, it may be supported by support rings and packing blocks as shown for the known arrangement in Figure 1.

A possible process for making the composite conductor will now be described with reference to Figure 5. At the left of Figure 5, many pre-insulated wire strands 31 of copper or other conductor material are drawn together from storage reels (not shown) and passed through a bundle forming head I to produce a conductor bundle 32. Within the head I are means, well known in the art of cable-making, whereby the strands 31 are brought together, formed into a bundle and the bundle is bodily twisted around the centreline of the bundle. At the same time as the strands 31 are being formed into a bundle, the bundle is impregnated with an epoxy resin or similar binding and strengthening agent resistant to high temperatures; alternatively, this impregnation process may be a pressure impregnation process, as known, the pressure impregnation being accomplished immediately after the conductor bundle has been formed and either within the head I or following it. The final process within head I (which may in practice be carried out in a separate head, not shown) is to finally form and consolidate the conductor bundle into the required rectangular shape of the present invention by passing it through a suitably shaped die.

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The head I is heated so as to partially cure the resin as the conductor bundle passes therethrough, thereby producing a conductor bundle which has good cohesion, yet is still sufficiently flexible to be wound onto a large diameter storage drum S1 for later use. Alternatively, the partly cured bundle passes straight on as indicated through the centre of an annular die in extruding head II, whereby a conductive filled polymer film is extruded onto the outside of the conductor bundle 32 to form a first, inner, corona shield. Thereafter, the coated conductor bundle passes through the centre of a further annular die in extruding head III, whereby a filled polymer insulating sleeve is extruded onto the outside of the first corona shield. Effectively, this first corona shield thereby forms a conductive coating on the inner surface of the insulating sleeve. Finally, by a similar process to that described for head II, a second, outer, corona shield is applied to the insulating sleeve in extruding head IV, so completing the formation of a composite conductor 30. The composite conductor 30 can then be wound onto a large diameter storage drum S2 for later use. Alternatively, as indicated by the dashed arrow line, it can pass straight into a further manufacturing stage for producing windings for electrical machines. As mentioned previously, final curing of the conductor bundles is accomplished by heating, after the composite conductor has been fixed into the winding slots in an electrical machine, as shown in Figure 4.

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It has been said above that the wire strands 31 are pre-insulated, meaning that during their manufacture they have been provided with a thin coating of suitable epoxy resin or high temperature resistant polymer, as known. However, as an alternative to the use of pre-insulated wire strands, it may be possible to rely on the resin impregnation process which occurs in head I to insulate the strands 31 from each other within the finished conductor bundle. This will be a matter for determination by routine experimentation.

25

Although in Figure 5 the strands are shown being gathered together into a bundle in a one-stage process, in practice, due to the large number of strands required to make a

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conductor bundle, this first part of the process may require a number of parallel stages in which a number of sub-bundles are produced in corresponding bundle-producing heads, each bundle having been impregnated with resin therein as described previously, the sub-bundles then being brought together to form the final twisted rectangular conductor bundle 32.

It will be evident that the above process may be used to produce composite conductors having cross-sectional shapes other than rectangular, e.g. circular.

CLAIMS

1. A composite conductor for use as a winding of a high voltage electrical machine, comprising:

5 a plurality of strands of conductor material forming a conductor bundle which in cross-section is of generally rectangular shape, the strands being insulated from each other within the bundle,

an insulating sleeve of substantially homogeneous polymeric material surrounding the conductor bundle; the insulating sleeve also having a generally
10 rectangular shape in cross-section and the polymeric material being filled with at least one electrically insulating filler material which conducts heat more efficiently than the polymer alone, and

conductive material forming a corona shield coating at the inner and outer surfaces of the insulating sleeve.

15

2. A composite conductor according to claim 1, the corners of the conductor bundle's rectangular shape being radiused to minimise electrical stress concentrations.

3. A composite conductor according to claim 2, the radius dimensions of the
20 corners of the conductor bundle being up to about 5 mm.

4. A composite conductor according to claim 3, the radius dimensions being between 2-3 mm.

25 5. A composite conductor according to any preceding claim, the corners of the insulating sleeve being substantially rectilinear.

6. A composite conductor according to claim 5, the corners of the insulating sleeve having a radius of not more than about 1mm.

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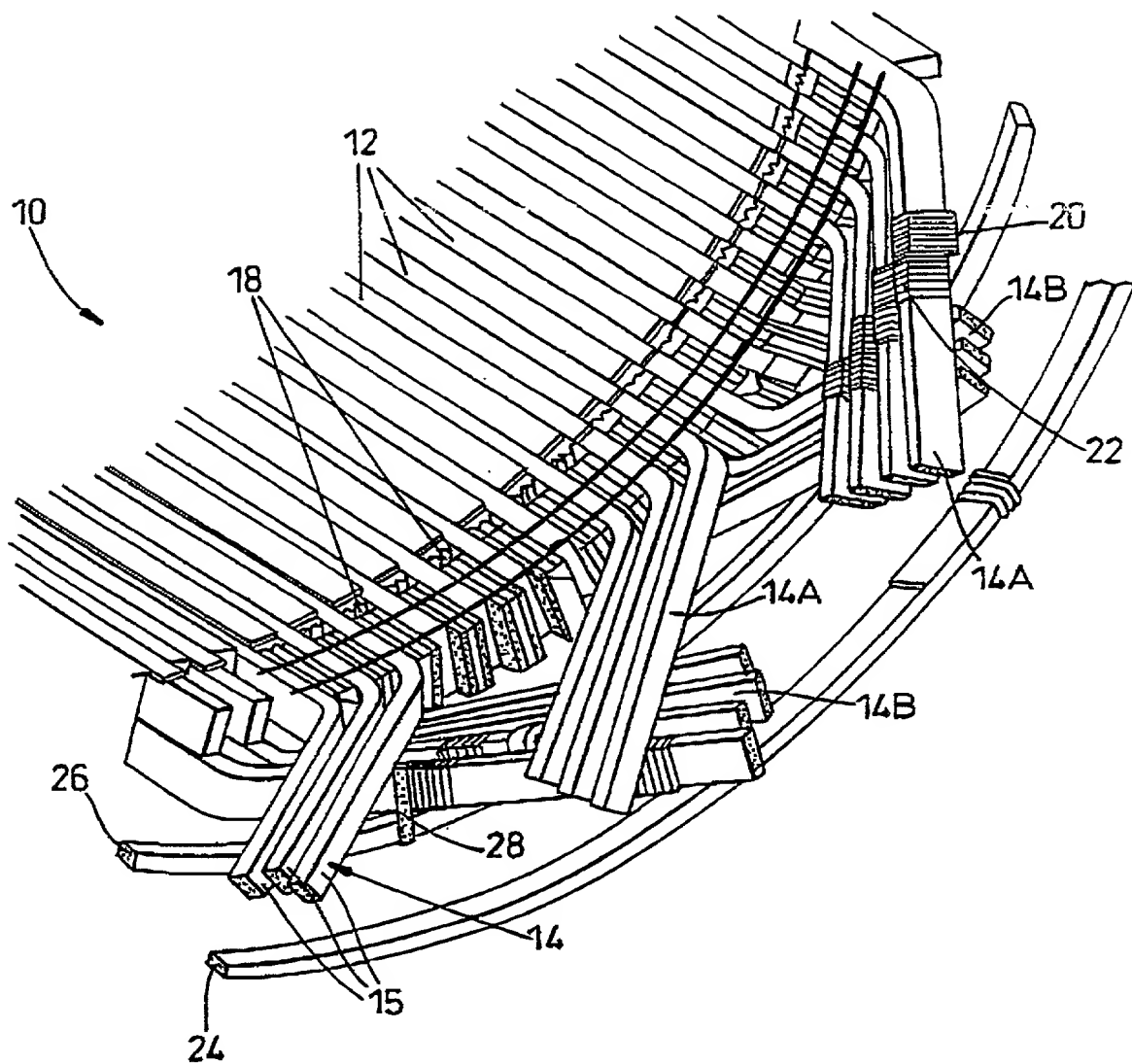


Fig. 1

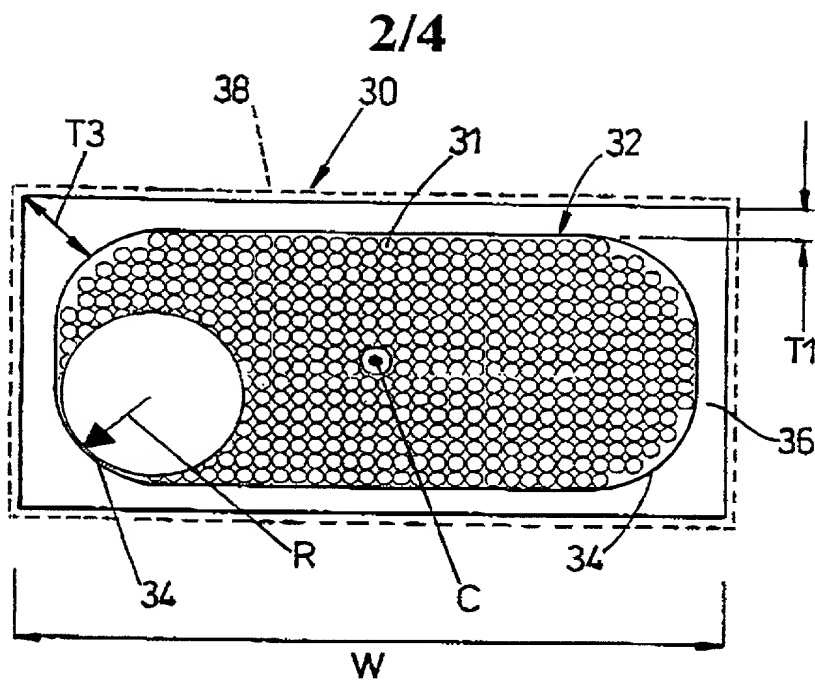


Fig. 2

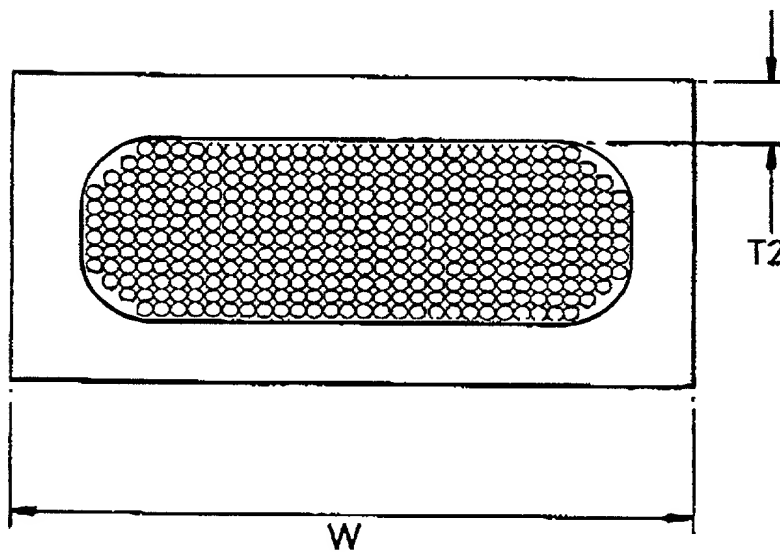


Fig. 3

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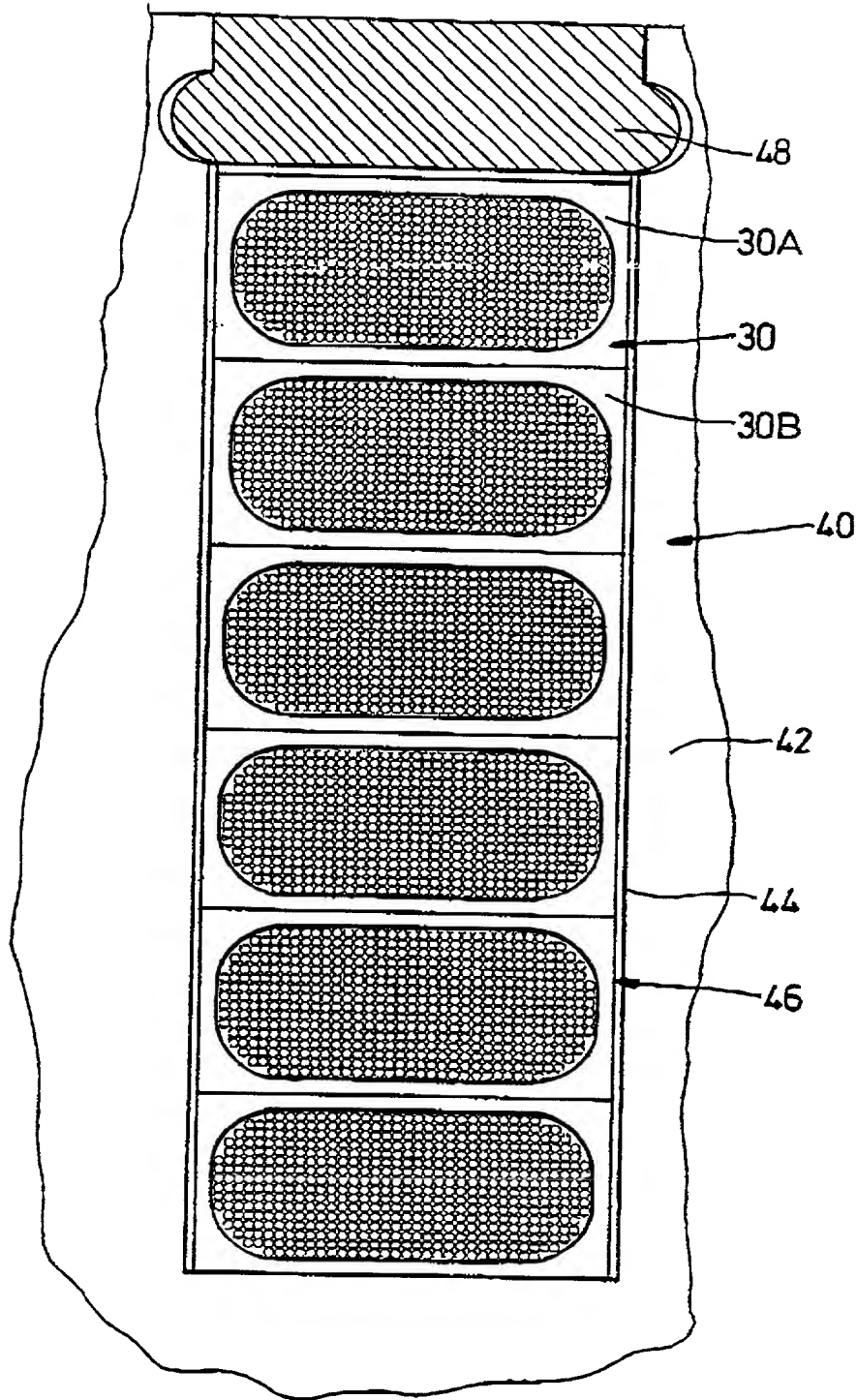


Fig. 4

SUBSTITUTE SHEET (RULE 26)

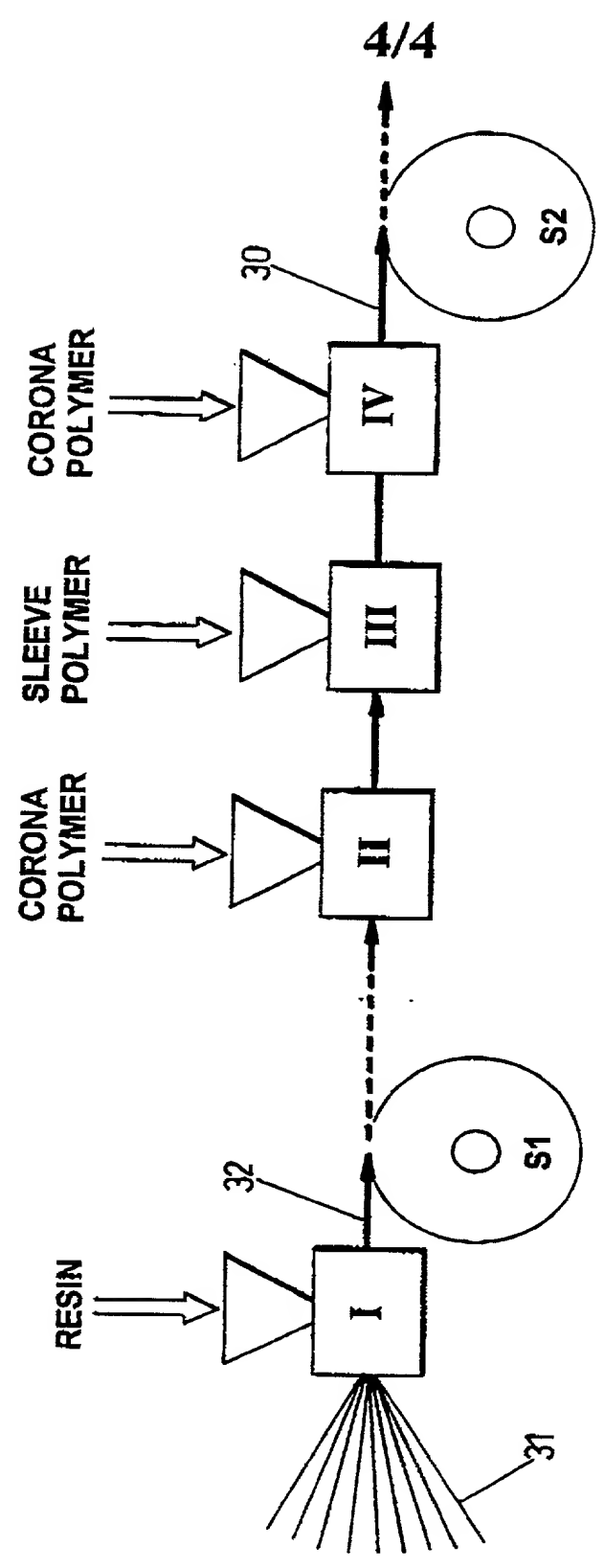


Fig. 5

PATENT APPLICATION

DECLARATION AND POWER OF ATTORNEY
FOR PATENT APPLICATION

ATTORNEY DOCKET NO. P/70017ALSTOM

As a below named inventor, I hereby declare that:

My residence/post office address and citizenship are as stated below next to my name;

I believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the invention entitled:

IMPROVEMENTS IN ELECTRICAL MACHINES

the specification of which is attached hereto unless the following box is checked:

(X) was filed on **September 28, 2001** as US Application Serial No. or PCT International ApplicationNumber 09/937,746 and was amended on _____ (if applicable).

I hereby state that I have reviewed and understood the contents of the above-identified specification, including the claims, as amended by any amendment(s) referred to above. I acknowledge the duty to disclose all information which is material to patentability as defined in 37 CFR 1.56.

Foreign Application(s) and/or Claim of Foreign Priority

I hereby claim foreign priority benefits under Title 35, United States Code Section 119 of any foreign application(s) for patent or inventor(s) certificate listed below and have also identified below any foreign application for patent or inventor(s) certificate having a filing date before that of the application on which priority is claimed:

COUNTRY	APPLICATION NUMBER	DATE FILED	PRIORITY CLAIMED UNDER 35 U.S.C. 119
United Kingdom	9907527.7	April 1, 1999	YES: X NO:
International	PCT/GB00/01112	March 31, 2000	YES: X NO:

Provisional Application

I hereby claim the benefit under Title 35, United States Code Section 119(e) of any United States provisional application(s) listed below:

APPLICATION SERIAL NUMBER	FILING DATE

U.S. Priority Claim

I hereby claim the benefit under Title 35, United States Code, Section 120 of any United States application(s) listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States application in the manner provided by the first paragraph of Title 35, United States Code Section 112, I acknowledge the duty to disclose material information as defined in Title 37, Code of Federal Regulations, Section 1.56(a) which occurred between the filing date of the prior application and the national or PCT international filing date of this application:

APPLICATION SERIAL NUMBER	FILING DATE	STATUS(patented/pending/abandoned)

POWER OF ATTORNEY:

As a named inventor, I hereby appoint the following attorney(s) and/or agent(s) listed below to prosecute this application and transact all business in the Patent and Trademark Office connected therewith.

Alan Israel, Reg. No. 27564

Send Correspondence to:	Direct Telephone Calls To:
Alan Israel Kirschstein, Ottinger, Israel & Schiffmiller, P.C. 489 Fifth Avenue New York, NY 10017-6105	Alan Israel 212-697-3750

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

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Inventor's Signature

Date

22 Oct. 2001